

3. PROXIMITY SENSOR

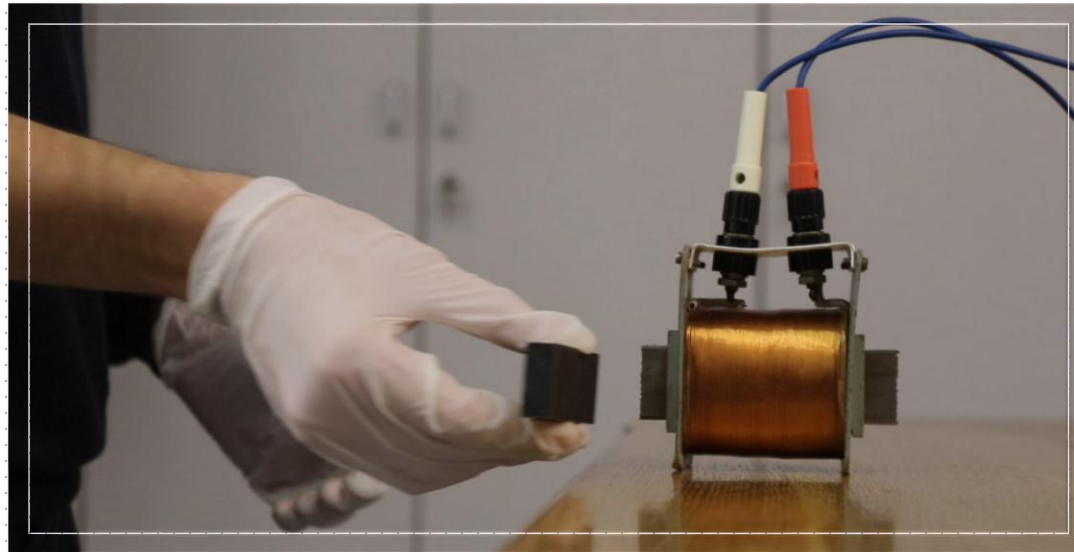
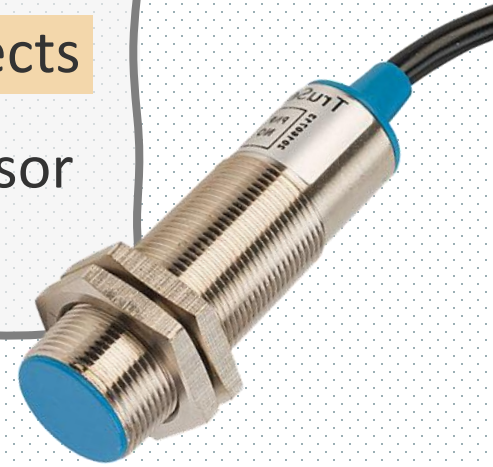
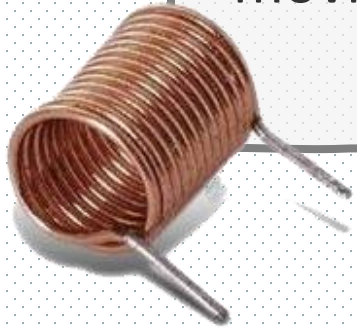
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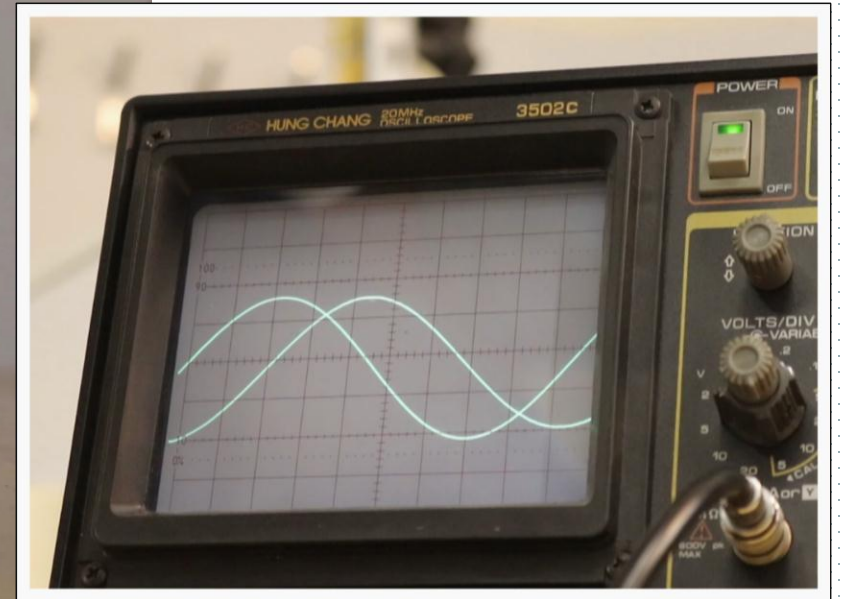
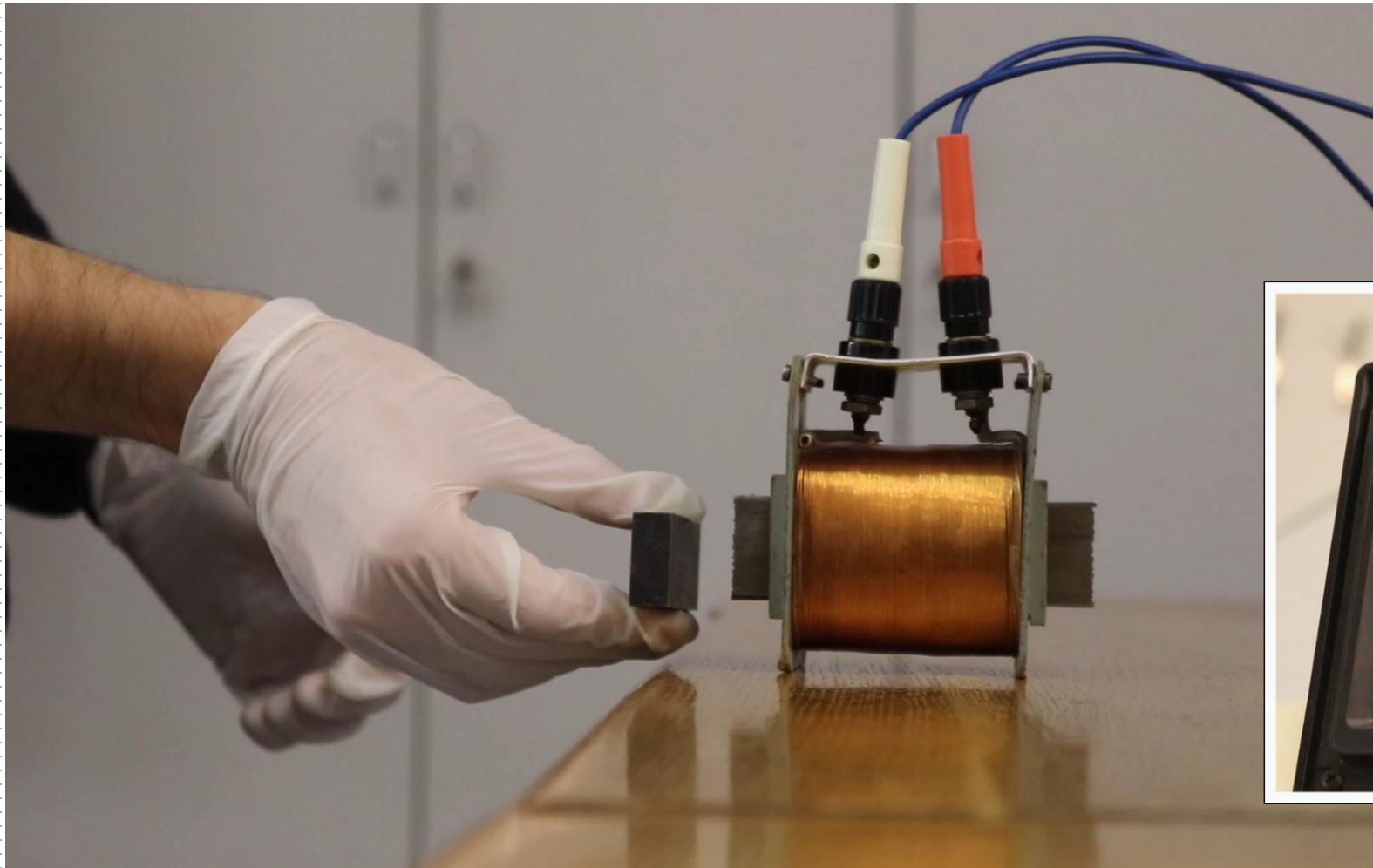


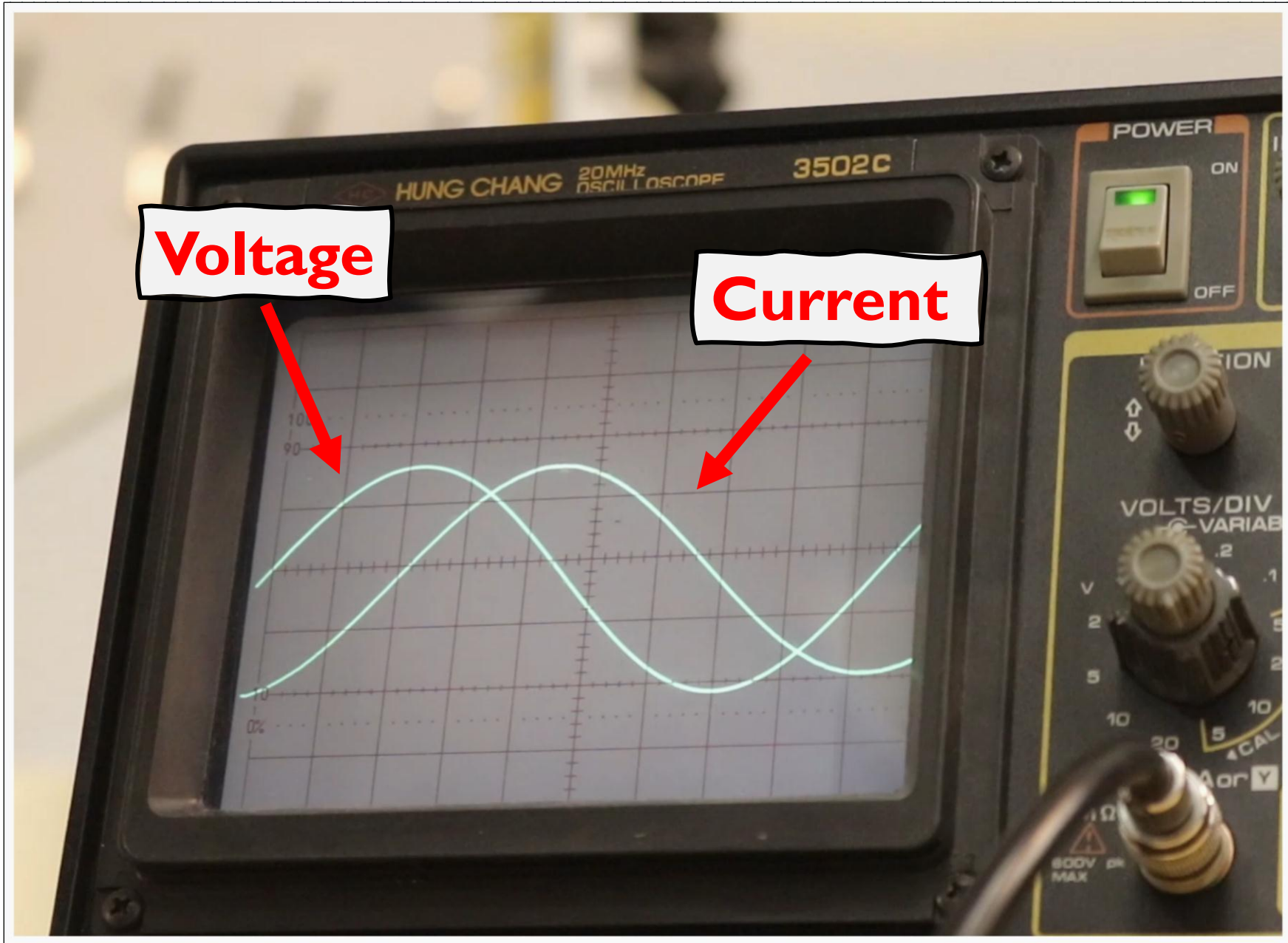
Proximity Sensor

A simple passive inductive sensor can detect ferromagnetic objects moving through its magnetic field. Construct such a passive sensor and investigate its characteristics such as sensing range.



DEMONSTRATION



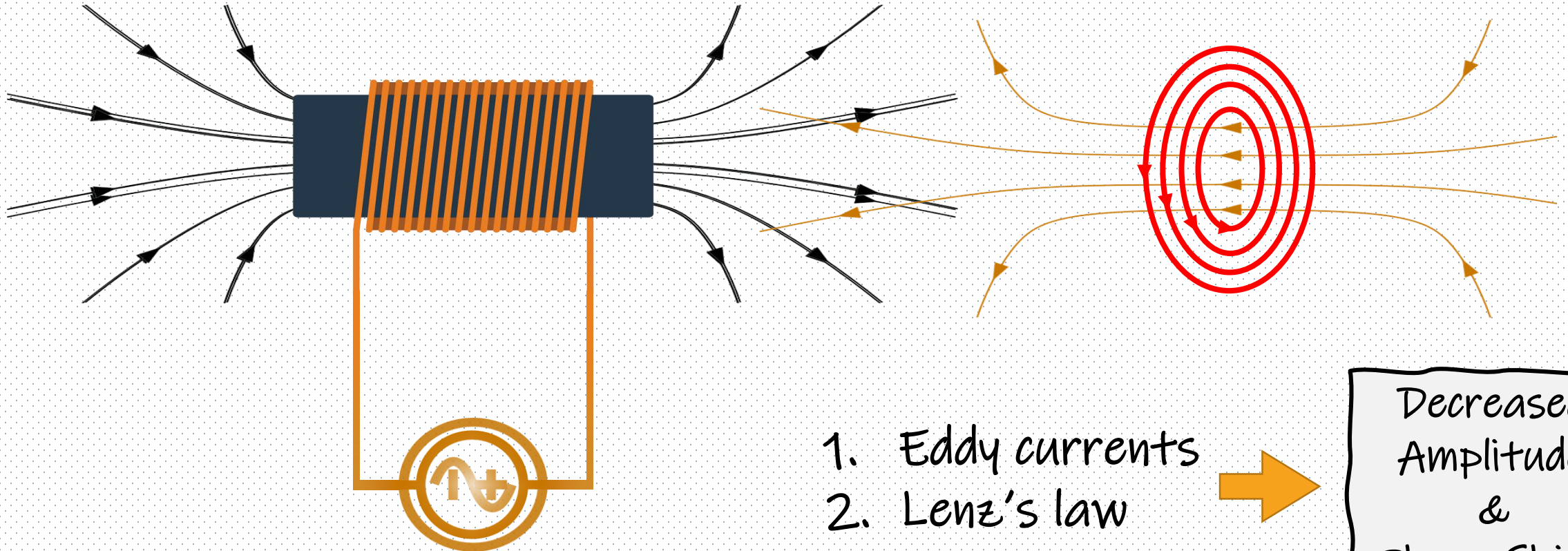


Voltage

Current

BASIC EXPLANATION

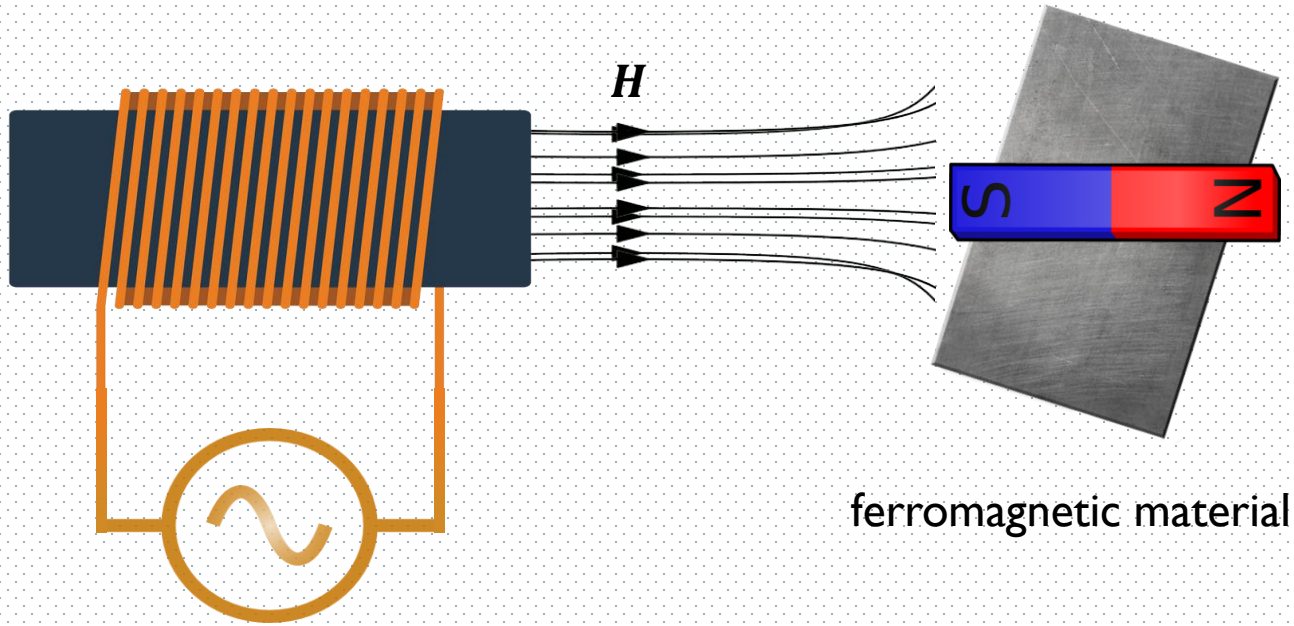
I. effect – Eddy currents



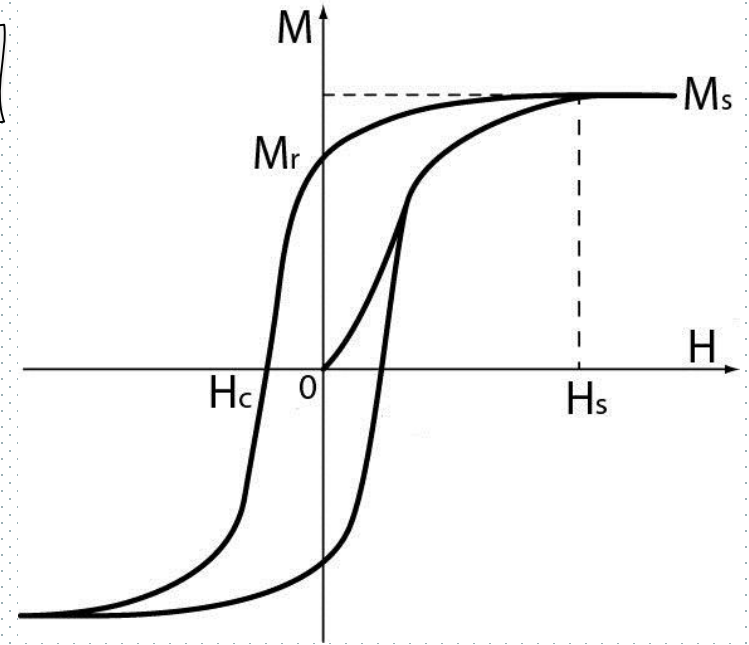
1. Eddy currents
2. Lenz's law

Decreased
Amplitude
&
Phase Shift

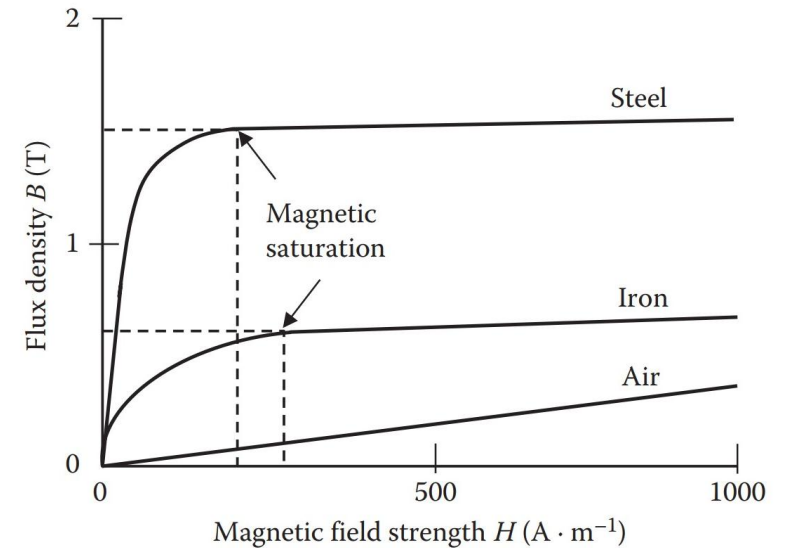
II. effect - Magnetization of the ferromagnetic material

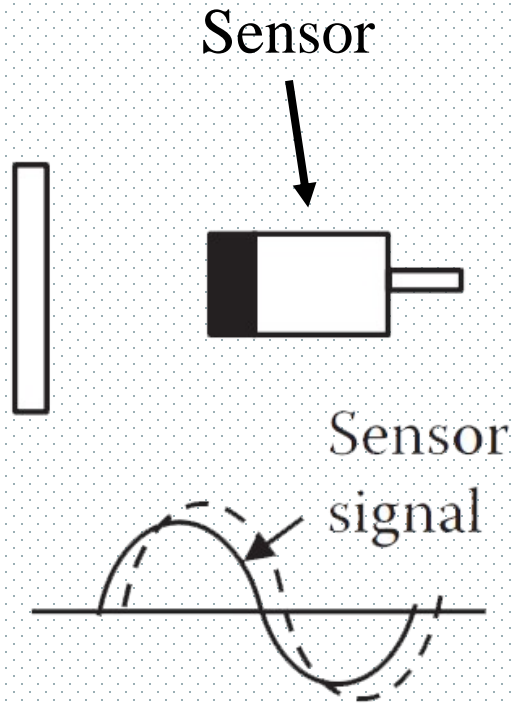


Φ increases $\rightarrow L = \frac{\Phi}{I}$ increases \rightarrow **frequency decreases**

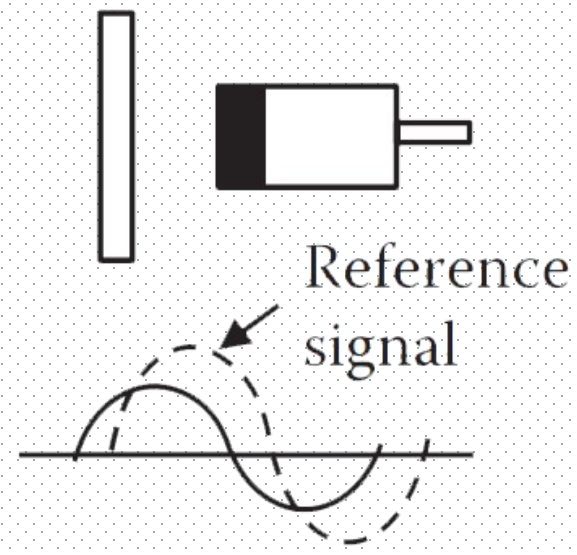


Hysteresis loop of magnetization

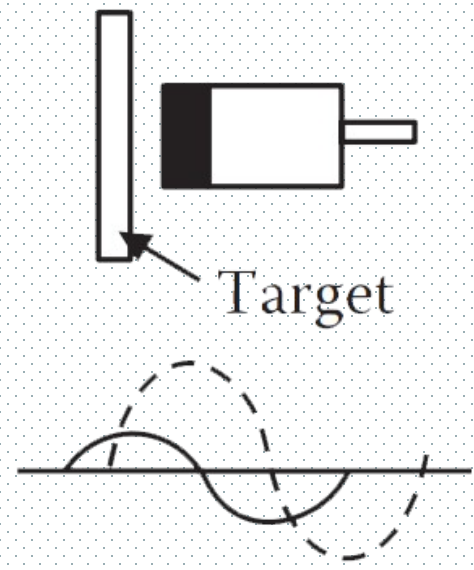




Distance: long
 Amplitude: large
 Phase difference: small



Distance: middle
 Amplitude: middle
 Phase difference: middle



Distance: short
 Amplitude: small
 Phase difference: large

POSSIBLE THEORETICAL CONSIDERATIONS

I., Using power dissipation of Eddy currents

$$P = \frac{\pi^2 B^2 d^2 f^2 V}{6\rho k} \quad [1]$$

P is the power lost (W),

B is the peak magnetic field (T),

d is the thickness of the sheet or diameter of the wire (m),

f is the frequency (Hz),

k is a constant (1 - thin sheet, 2 - thin wire)

ρ is the resistivity of the material ($\Omega \text{ m}$)

V is the volume of the material (kg/m^3).

The **voltage** and **current** of the inductor: $U(t) = U_0 \cdot \sin \omega t$ $I(t) = I_0 \cdot \cos \omega t$

$$P = \frac{\pi^2 B^2 d^2 f^2 V}{6\rho k} = c_1 \cdot B^2 = c_1 \cdot c_2 \cdot I_0^2 \cdot \cos^2(\omega t)$$

c_2 depends on the distance of the target! $c_2(d)$

Energy loss due to eddy currents in a quarter cycle:

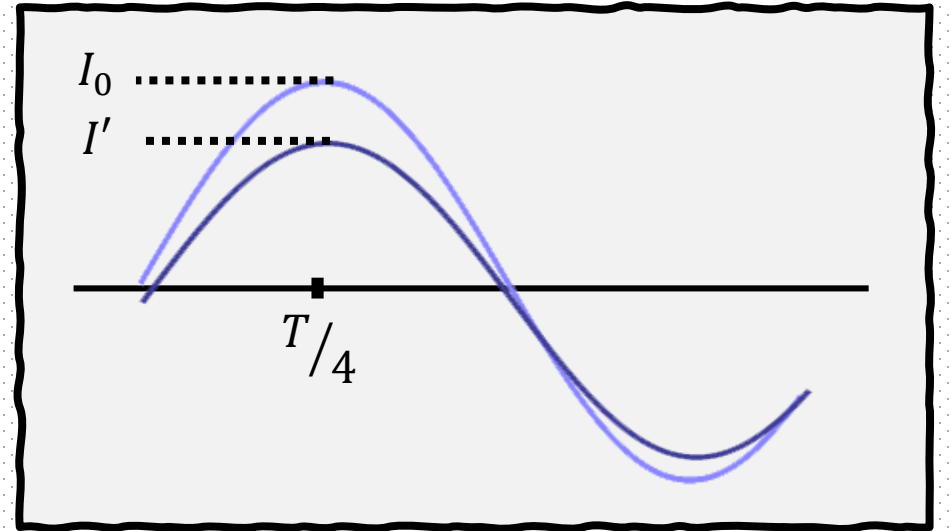
$$W_{loss} = \frac{\pi c_1 c_2}{4\omega} \cdot I_0^2 = K \cdot I_0^2$$

K depends on the distance of the target! $K(d)$

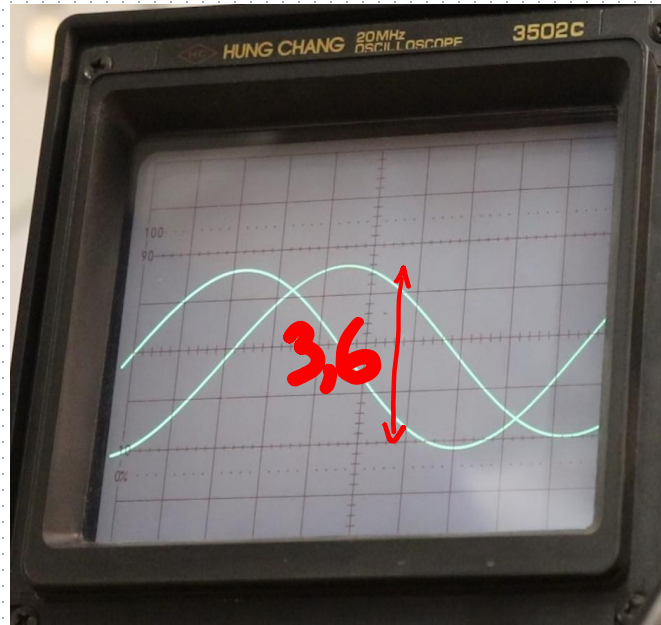
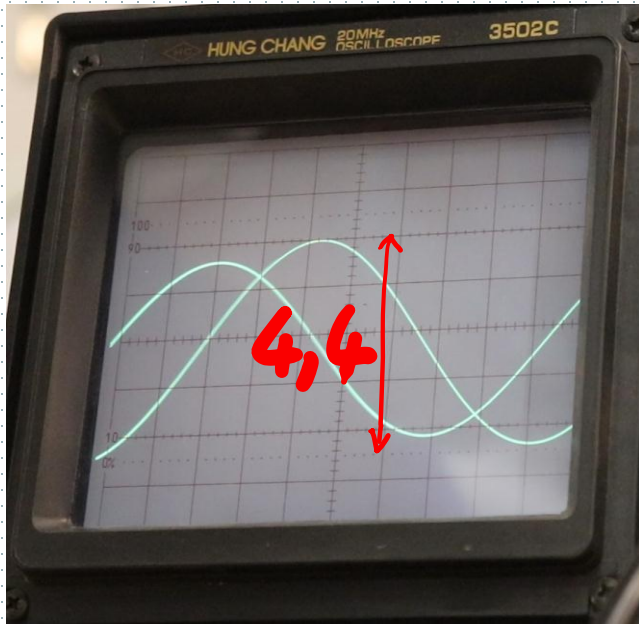
Inductor's change of energy:

$$\Delta W_{ind} = W_0 - W' = \frac{1}{2} L I_0^2 - \frac{1}{2} L I'^2 = \frac{1}{2} L (I_0^2 - I'^2)$$

$$W_{loss} = \Delta W_{ind} = \frac{1}{2} L (I_0^2 - I'^2) = K \cdot I_0^2$$



$$\frac{I'}{I_0} = \sqrt{1 - \frac{\pi c_1 c_2}{2L\omega}}$$



Measured decrease:

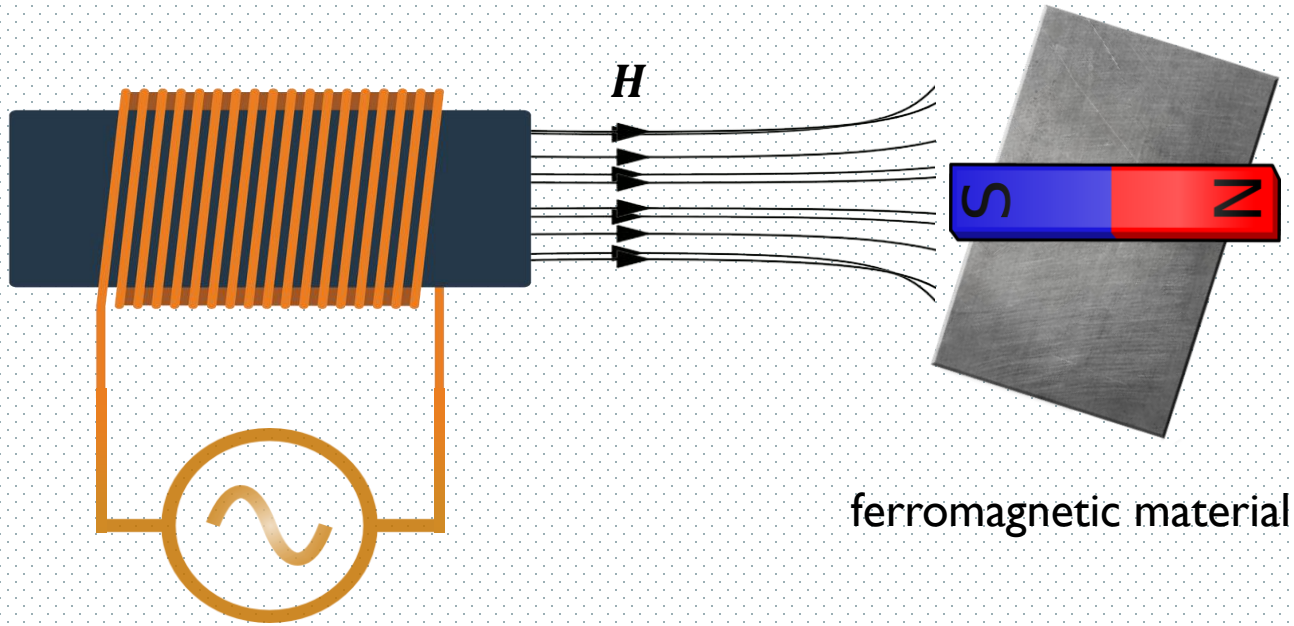
$$\frac{I_1}{I_0} = \frac{3.6}{4.4} = 0.82 \pm 0.08$$

Theoretical:

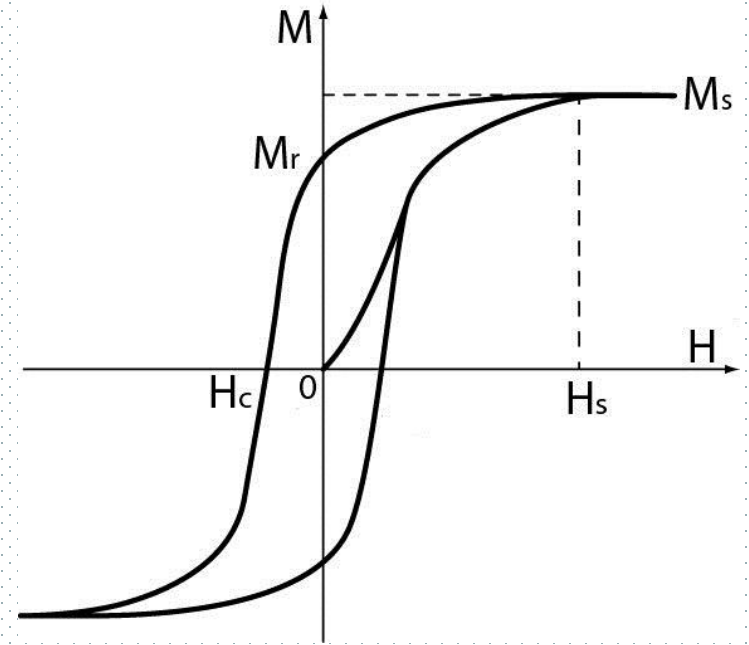
$$\frac{I_1}{I_0} = \sqrt{1 - \frac{\pi C_1 C_2}{2L\omega}} = \sqrt{1 - \frac{\pi^2 d^2 f V \mu_0 \mu_r n}{24k\rho L}} = 0.966$$

$$d \rightarrow 0.01 \text{ m}, f \rightarrow 100 \frac{1}{\text{s}}, V \rightarrow 0.06 \cdot 0.02 \cdot 0.01 \text{ m}^3, \rho \rightarrow 9.7 \cdot 10^{-8} \Omega \text{ m}, k \rightarrow 1, L \rightarrow 4.5 \text{ H}, \mu_r \rightarrow 50, N \rightarrow 1200,$$

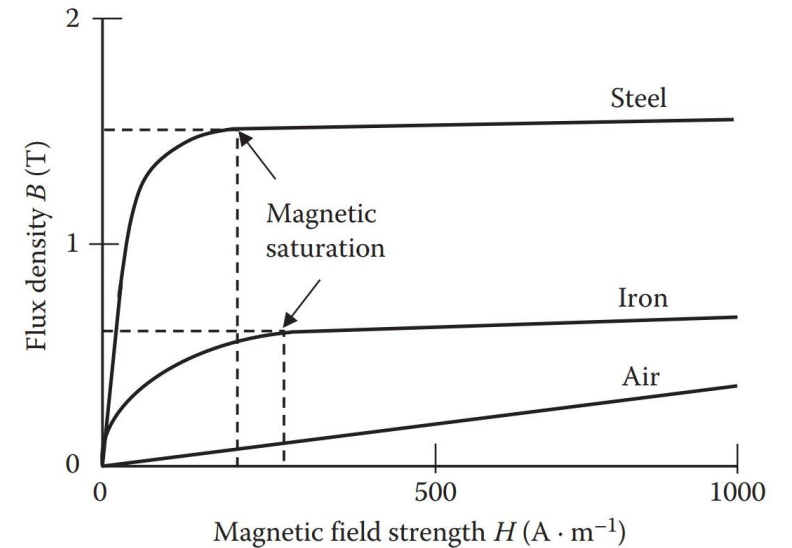
II., Change of inductance



Φ increases $\rightarrow L = \frac{\Phi}{I}$ increases \rightarrow **frequency decreases**



Hysteresis loop of magnetization

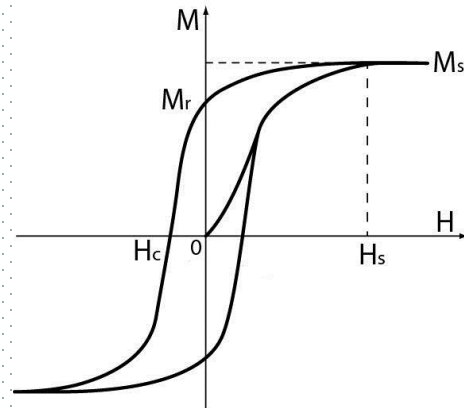


Magnetic field strength at the end of a solenoid:

$$H = \frac{IN}{l} \cdot \frac{l}{2\sqrt{r^2 + l^2}}$$



M magnetization



B_{magnet}



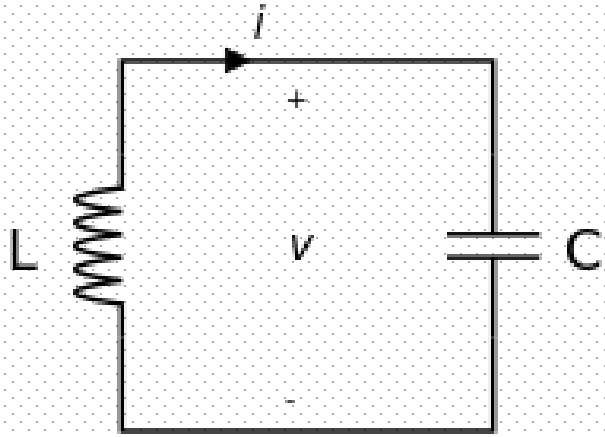
$$\Delta\Phi = N \int B_{\text{magnet}} dA$$

magnetic flux change inside the solenoid



$$L = \frac{\Phi + \Delta\Phi(d)}{I} = \frac{\mu N^2 A}{l} + \frac{\Delta\Phi}{I} = L_0 + \frac{\Delta\Phi}{I}$$

LC circuit:

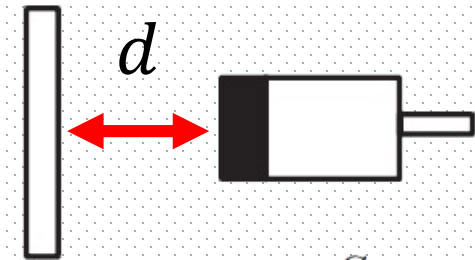


$$L = L_0 + \frac{\Delta\Phi}{I}$$

$$\omega = \sqrt{1/LC} = \sqrt{\frac{1}{C(L_0 + \frac{\Delta\Phi}{I})}} < \omega_0$$

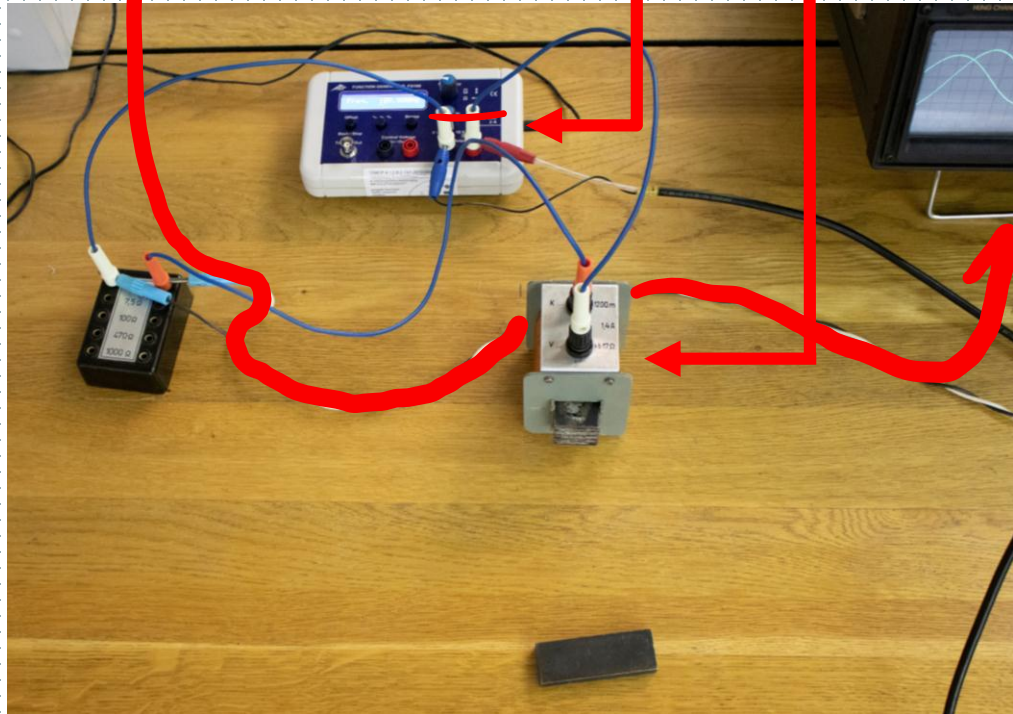
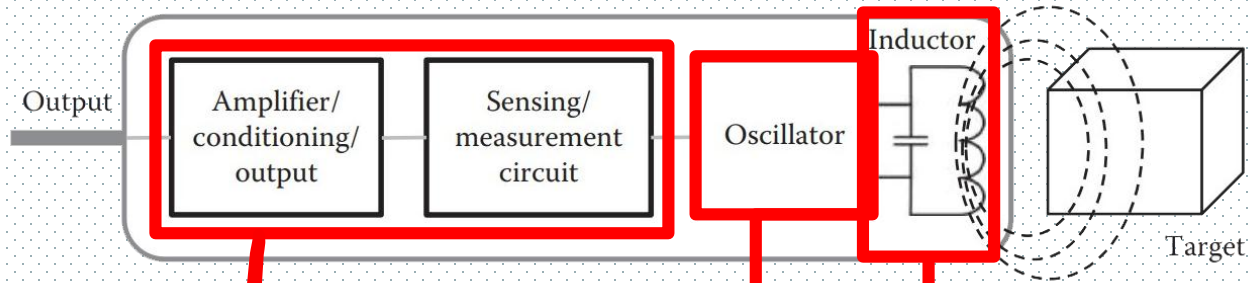
$\Delta\Phi$ is dependent on the distance of the subject (d)!

$$d_1 < d_2 \rightarrow \Delta\Phi_1 > \Delta\Phi_2$$



Given the $\delta\omega$ (the **precision** of the measuring device) a formula for **sensing range** can be calculated.

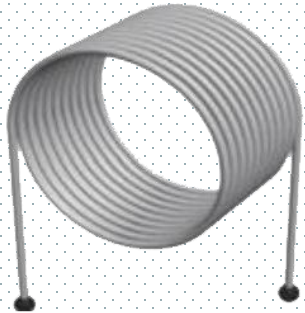
SETUP



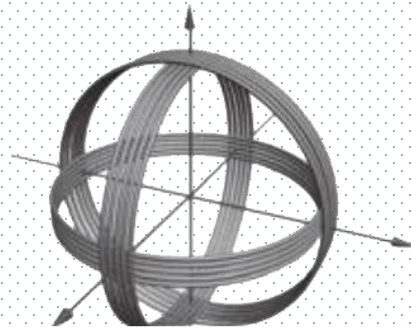
oscilloscope

Air Coil

- + light, stable, durable
- + no hysteresis loss
- limited sensitivity (low inductance)



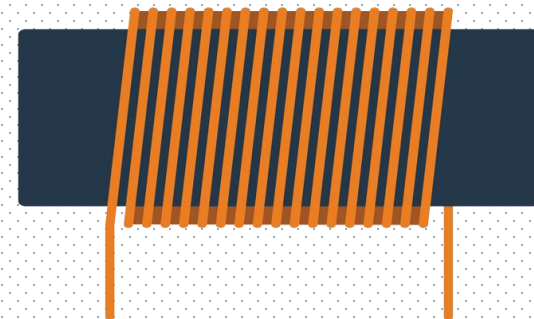
Single-coil sensor

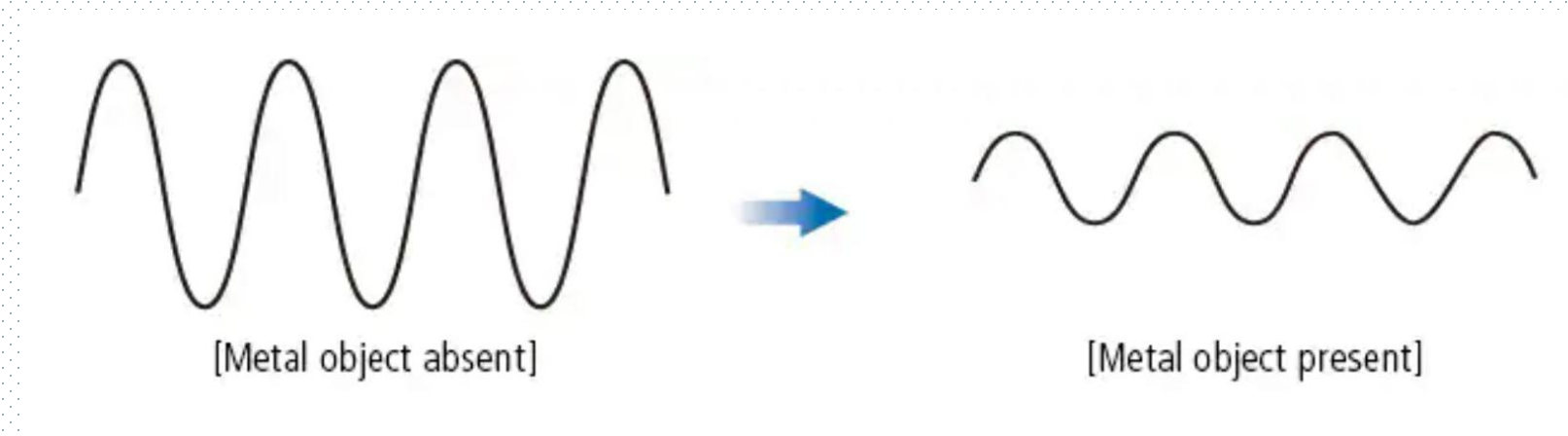


Three mutually perpendicular coils

Ferromagnetic core

- + higher sensitivity
- less stable, nonlinear
- more energy loss



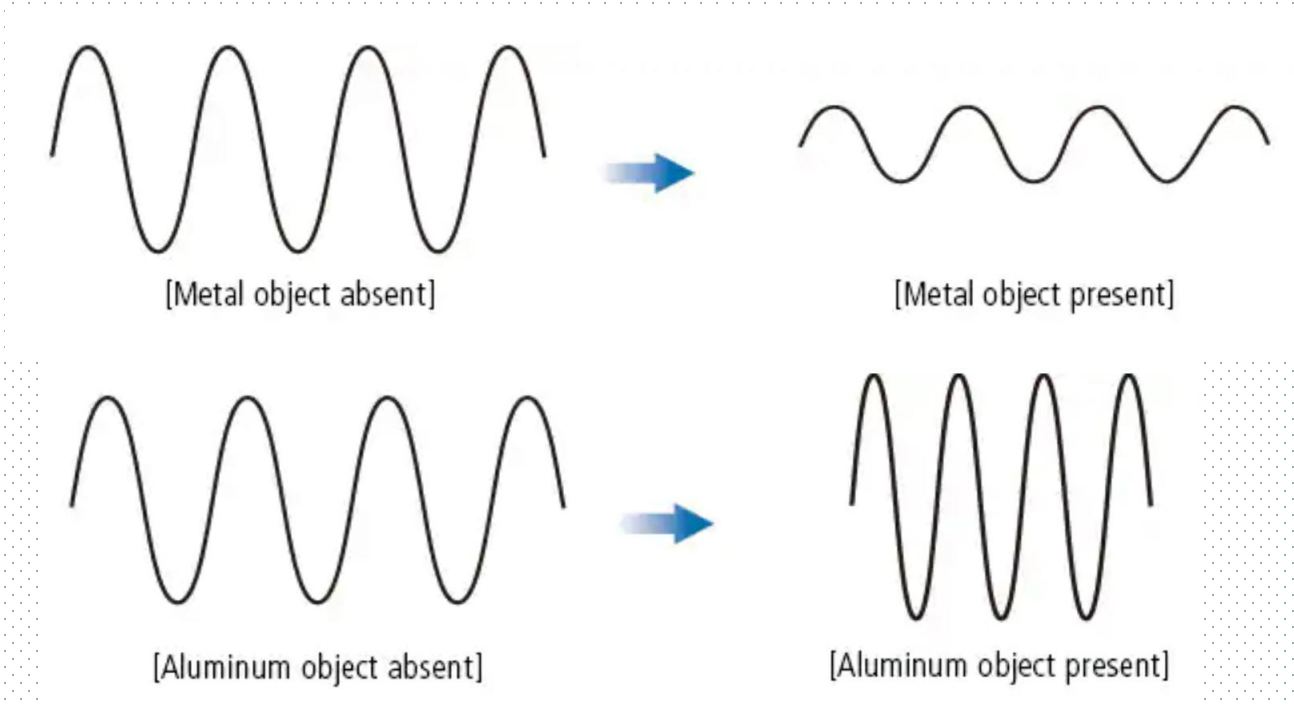


Measuring frequency (f) \rightarrow reaches threshold value \rightarrow LED turns on

SOURCES, REFERENCES

- Winncy Y. Du, *Resistive, Capacitive, Inductive, and Magnetic Sensor Technologies*, Chapter 4 *Inductive Sensors*
- What is an Inductive Proximity Sensor? (available at: <https://www.keyence.com/ss/products/sensor/sensorbasics/proximity/info/>)
- S. Tumanski, *Induction Coil Sensors* (available at: <http://www.tumanski.x.pl/coil.pdf>)
- Griffiths D. J., *Introduction to Electrodynamics*, Cambridge University Press, 2017.

THANK YOU FOR YOUR ATTENTION.



| | | | |
|---|--------------------|---------|-----------------------|
| Magnetism | Strong ←————→ Weak | | |
| Detecting distance of general-purpose model | Long ←————→ Short | | |
| Detecting distance of aluminum detection model | Short —————→ Long | | |
| Typical metal | Iron/SUS440 | SUS304* | Aluminum/brass/copper |

* SUS304 has an intermediate property.

The **voltage** and **current** of the inductor: $U(t) = U_0 \cdot \sin \omega t$ $I(t) = I_0 \cdot \cos \omega t$

$$P = \frac{\pi^2 B^2 d^2 f^2 V}{6\rho k} = c_1 \cdot B^2 = c_1 \cdot c_2 \cdot I_0^2 \cdot \cos^2(\omega t)$$

Energy loss due to eddy currents in a quarter cycle:

$$W_{\frac{1}{4}loss} = \int_{-\frac{\pi}{2\omega}}^0 P \cdot dt = c_1 \cdot c_2 \cdot I_0^2 \int_{-\frac{\pi}{2\omega}}^0 \cos^2(\omega t) \cdot dt = \frac{\pi c_1 c_2}{4\omega} \cdot I_0^2$$

Inductor's change of energy meanwhile:

$$\Delta W_{ind} = \frac{1}{2} L I_1^2 = \frac{1}{2} L I_0^2 - W_{\frac{1}{4}loss} = I_0^2 \left(\frac{1}{2} L - \frac{\pi c_1 c_2}{4\omega} \right)$$

$$\frac{I_1}{I_0} = \sqrt{1 - \frac{\pi c_1 c_2}{2L\omega}}$$